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## TITLE

### AUTOMATIC ADJUSTMENT SYSTEM FOR SOURCE CURRENT AND SINK CURRENT MISMATCH

## BACKGROUND OF THE INVENTION

### 5 Field of the Invention

The invention relates to an automatic adjustment system for source current and sink current mismatch, which implements a control reference table, such that a determination device and a current compensation device  
10 accordingly perform desired compensation for source current and sink current mismatch.

### Description of the Related Art

In a typical transceiver IC for communication, a phase locked loop (PLL) synthesizer is widely used. As shown in  
15 Fig. 1, the PLL synthesizer essentially includes a reference oscillator 10 and a reference divider 11 to provide a reference frequency  $F_{ref}$ ; a voltage-controlled oscillator 14 and a main divider 13 to provide a main frequency  $F_{main}$ ; a phase detector 12 and a loop filter 15 to produce a feedback  
20 frequency  $F_{back}$  by comparing the reference and main frequencies and output the feedback frequency  $F_{back}$  to the oscillator 14 to further produce an operating frequency  $F_{out}$  to be output.

However, as cited, the PLL synthesizer has some  
25 problems such as phase noises, non-linear effects, reference spurs and the like. One source of problems is source current flowing to the loop filter 15 being mismatched to

sink current flowing from the filter 15. Therefore, a desired charge pump circuit is needed to overcome the current mismatch problem.

#### **SUMMARY OF THE INVENTION**

5 It is an object of the present invention to provide an automatic adjustment system for source current and sink current mismatch, which automatically adjusts source current and sink current mismatch to reduce phase noise.

The present invention is generally directed to an  
10 automatic adjustment system for source current and sink current mismatch, which automatically adjusts source current and sink current mismatch to reduce spurs. The system includes a startup compensation/setup device to perform initialization current compensation and accordingly to  
15 implement a control reference table, a determination device to output a control signal according to the control reference table, and a current compensation device to switch corresponding internal switches on and off according to the control signal and complete the desired compensation for  
20 source current and sink current mismatch.

#### **DESCRIPTION OF THE DRAWINGS**

The present invention will be described by way of exemplary embodiments, but not limitations, illustrated in the accompanying drawings in which like references denote  
25 similar elements, and in which:

Fig. 1 is a block diagram of a typical PLL synthesizer;

Fig. 2 is a block diagram of an automatic adjustment system according to the invention;

Fig. 3 is a schematic diagram of the interior of a current compensation device of Fig. 2 according to the invention;

Fig. 4 is a schematic diagram of the interior of a startup compensation/setup device of Fig. 2 according to the invention; and

Fig. 5 is a schematic diagram of the interior of a determination device of Fig. 2 according to the invention.

#### DETAILED DESCRIPTION OF THE INVENTION

Fig. 2 is a block diagram of an automatic adjustment system according to the invention. In Fig. 2, the system essentially includes a startup compensation compensation/setup device 22, a determination device 23 and a current compensation device 21. A switch S1 is implemented between the devices 21 and 22 for connection and another switch S2 is implemented between the devices 22 and 23 for connection.

As shown in Fig. 2, when the system is provided with an external voltage VCC, on the feature difference between P-type and N-type semiconductor devices, a constant current, namely source current  $I_{sr}$ , is generated between the voltage VCC and a middle point M, and another constant current, namely sink current  $I_{sk}$ , is generated between the middle point M and a grounding terminal GND. Generally, the two currents  $I_{sr}$  and  $I_{sk}$  are the same and balance, such that a stable operating current and voltage are provided to the subsequent low pass filter (LPF) 24 and voltage-controlled oscillator 25 for use. However, due to communication specification requirements of heat, phase margin and the

like, the source and sink currents  $I_{sr}$  and  $I_{sk}$  are physically not the same. At startup, the switch  $S1$  is closed to turn on the device 22 for startup compensation. The startup compensation can be performed directly through  
5 the control device 21 itself (dotted line) or indirectly through the device 23 to output a control signal  $Sc$  for controlling the device 21 after the switch  $S2$  is closed (solid line). After the startup compensation is completed, the device 22 sets up a reference index to generate a logic  
10 control table. As soon as the logic control table is completed, the switch  $S1$  is opened to protect the system from the startup compensation again, affecting the entire operation.

As shown in Fig. 2, when a mismatch between the  
15 currents  $I_{sr}$  and  $I_{sk}$  occurs, the device 23 outputs a logical control signal to the device 21 according to the logic control table. The device 21 then performs current adjustment according to the logical control signal, accordingly achieving the automatic adjustment. Interiors  
20 for the devices are further described in the following.

Fig. 3 is a schematic diagram of the interior of a current compensation device 21 of Fig. 2 according to the invention. In Fig. 3, the current compensation device 21 includes a plurality of first switches  $SW11-SW1N$ , a  
25 plurality of first constant current sources  $I11-I1N$  connected in series to the first switches one to one, a plurality of second switches  $SW21-SW2N$ , and a plurality of second constant current sources  $I21-I2N$  connected in series to the second switches one to one, wherein the first  
30 constant current sources respectively have an input terminal

connected to the external voltage VCC, the second constant current sources respectively have a grounding output terminal, and the switches SW11-SW2N respectively have an open terminal connected to a transmission line L to form a  
5 railing implementation. One end of the transmission line L is connected to the device 25 through the filter 24 and the other is connected to the point M (Fig. 2).

As shown in Fig. 3, when the voltage  $V_{tune}$  input to the device 25 is higher than a first predetermined value (while  
10 the source current  $I_{sr}$  is lower than the sink current  $I_{sk}$ ) at operation, a control signal  $S_c$  is input (described later) to close the corresponding first switches and accordingly to form current pathways such that the corresponding constant current sources flow to the transmission line L through the  
15 corresponding current pathways. The activation above starts the closing action from SW11 sequentially for sourcing the corresponding constant currents to increase the source current (or decrease the sink current) on the transmission line L, until the voltage  $V_{tune}$  input to the device 25 is  
20 lower than the first predetermined value (while  $I_{sr} = I_{sk}$ ). Similarly, when the voltage  $V_{tune}$  input to the device 25 is lower than a second predetermined value (while the source current  $I_{sr}$  is higher than the sink current  $I_{sk}$ ) at operation, the control signal  $S_c$  is input (described later)  
25 to close the corresponding second switches and accordingly form current pathways such that the corresponding constant current sources flow to the transmission line L through the corresponding current pathways. The activation above starts the closing action from SW21 sequentially for sinking the  
30 corresponding constant currents to decrease the sink current

(or increase the sink current) flowing on the transmission line L, until the voltage  $V_{tune}$  input to the device 25 is higher than the second predetermined value (while  $I_{sr} = I_{sk}$ ).

5        Fig. 4 is a schematic diagram of the interior of a startup compensation/setup device of Fig. 2 according to the invention. In Fig. 4, in order to provide current-calibrated compensation at startup and accordingly set the predetermined values, the startup compensation/setup device  
10 includes a detecting resistor  $R_t$ , an amplifier 41, an analog-to-digital converter 42 and a logic controller 43.

As shown in Fig. 4, the mismatch between the source and sink currents presents on two ends of the detecting resistor  $R_t$  in the form of different voltages (that is, different  
15 currents flowing to/from the resistor). Therefore, when current sources  $I_{sr}$ ,  $I_{sk}$  are initially turned on and the switch S1 is closed, the voltages  $V_{cp}$ ,  $V_{ref}$  on the two ends of the detecting resistor  $R_t$  are compensated (/determined) by the amplifier 41 and the converter 42 and converted into  
20 digital reference signals  $V_{t-H}$ ,  $V_{t-L}$ , input to the controller 43 to be stored. The compensation action is performed by directly input the signals  $V_{t-H}$ ,  $V_{t-L}$  to the device 21 for compensation, or input an output signal  $S_{out}$  to the device 23 to generate the control signal  $S_c$  (described later) after  
25 the controller 43 converts the signals  $V_{t-H}$ ,  $V_{t-L}$  into the output signal  $S_{out}$ . Further, the controller 43 can set the same or different compensation steps for current compensation in use of initialization.

Fig. 5 is a schematic diagram of the interior of a  
30 determination device of Fig. 2 according to the invention.

In Fig. 5, the determination device includes a bandgap reference circuit 55 to output a reference voltage  $V_t$ , a comparator 51 to compare the reference voltage  $V_t$  and the voltage  $V_{tune}$  input to the device 25 and accordingly  
5 generate a compare signal  $S_{comp}$ , and a selector 53 to generate the control signal  $S_c$  based on the compare signal  $S_{comp}$  in reference with the signal  $S_{out}$  output by the device 22.

As shown in Fig. 5, the signal  $S_{comp}$  is a differential  
10 value insufficiently determining source current or sink current and how much to compensate for the current match. Therefore, the table in the device 22 is provided with required references for current compensation. For example, in the device 21 for  $N=8$ , the signal  $S_{out}$  presents logic  
15 0001 representing closing the switch SW11 for source current compensation; 0010 representing closing the switches SW11 and SW12 for source current compensation, 0011 representing closing the switches SW11, SW12 and SW13 for source current compensation, and so on. As well, the signal  $S_{out}$  presents  
20 logic 1001 representing closing the switch SW21 for sink current compensation, 1010 representing closing the switches SW21 and SW22 for sink current compensation, 1011 representing closing the switches SW21, SW22 and SW23 for sink current compensation, and so on. In addition, the  
25 cited logical values can be converted by a digital-to-analog converter into stepped references (or implementing the digital-to-analog converter in the controller of the device 22 to be output directly as the signal  $S_{out}$ ). For example, logic 0001 represents a 0.001V to 1.0V output voltage, 0010  
30 for a 1.1V to 2.0V output voltage, 0011 for a 2.1V to 3.0V

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output voltage, 1001 for a 0.001V to -1.0V output voltage, 1010 for a -1.1V to -2.0V output voltage, 1011 for -2.1V to -3.0V output voltage, and so on. As cited, the invention achieves the purpose of source and sink current match.

5        While the invention has been described by way of example and in terms of the preferred embodiments, it is to be understood that the invention is not limited to the disclosed embodiments. To the contrary, it is intended to cover various modifications and similar arrangements (as  
10        would be apparent to those skilled in the art). Therefore, the scope of the appended claims should be accorded the broadest interpretation so as to encompass all such modifications and similar arrangements.